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TECHNICAL REPORT HSM-R114

METHODS  
OF  
DETERMINING THE SATURN I BUFFETING RESPONSE  
FROM RIGID MODEL WIND TUNNEL TESTS

VOLUME II

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SPACE DIVISION  CHRYSLER  
CORPORATION  
HUNTSVILLE OPERATIONS

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## ABSTRACT

The experimental determination of the buffeting on a launch vehicle is analyzed. The statistical prediction of the gross vehicle loadings and displacements from wind tunnel data obtained from rigid models is considered. The dynamic response of the vehicle in bending and in sloshing is described. Design of a wind tunnel test that will determine the required data is outlined. The instrumentation requirements are discussed. Data reduction techniques are described that generate the power spectral densities of the aerodynamic forcing. The scaling rules are included. Saturn I test data are reduced and the results compared with the results of an aeroelastic test and a flight test. The main portion of the report is contained in Volume I. The classified data and results are contained in Volume II.

This document contains information which is neither national defense nor intelligence information within the meaning of the espionage laws, Title 18, U.S.C., Sections 793 and 794, the transmission or communication of which in any manner to an unauthorized person is prohibited by law.

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Downgrade after 12 months; declassified after 12 years.

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## FOREWORD

This report was prepared by the Aero-Space Mechanics Branch, Structures & Mechanics Engineering Department, Huntsville Space Operations, Chrysler Corporation. The work was authorized by task assignment R-AERO-SAT-I-IB/1-65, work assignment AU-4, Contract NAS8-4016, issued by the Unsteady Aerodynamics Branch, Aerodynamics Division, Aero-Astroynamics Laboratory, Marshall Space Flight Center. The purpose of this study is to establish the data reduction procedures for wind tunnel buffeting tests conducted with rigid models. Saturn I data are reduced and compared with the results of an aeroelastic test and with flight test data. Suggestions are made concerning the design of rigid model tests.

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## INTRODUCTION

A study has been made to determine methods for reducing wind tunnel buffeting data taken with rigid models. Data from a series of Saturn I tests, designated PSTL-1, were reduced by these methods. They are compared with those of an aeroelastic model test and a flight test of the Saturn. The analysis is contained in Vol. I, which is unclassified. The PSTL-1 tests are classified despite the fact that the aeroelastic tests and the buffeting data from the flight tests are not classified. The PSTL-1 data are given in Vol. II, which is classified.

The bending moments generated by buffeting are determined by the cross spectrum method. They are shown in figures 1 through 8. The limits of the bending deflections are shown in figures 9 through 12. A comparison of the computed and measured RMS pitching moment coefficients is given in figure 13. The power spectral densities of the moments are given in figure 14 and 15. The local normal force coefficients measured in the PSTL-1 tests are shown in figure 16. The minimum and maximum PSTL-1 bending moment distributions are compared with the bending moment distributions obtained in the aeroelastic test in figures 17 and 18. The vehicle deflection at the instrumentation unit during a Saturn flight is given in figure 19.

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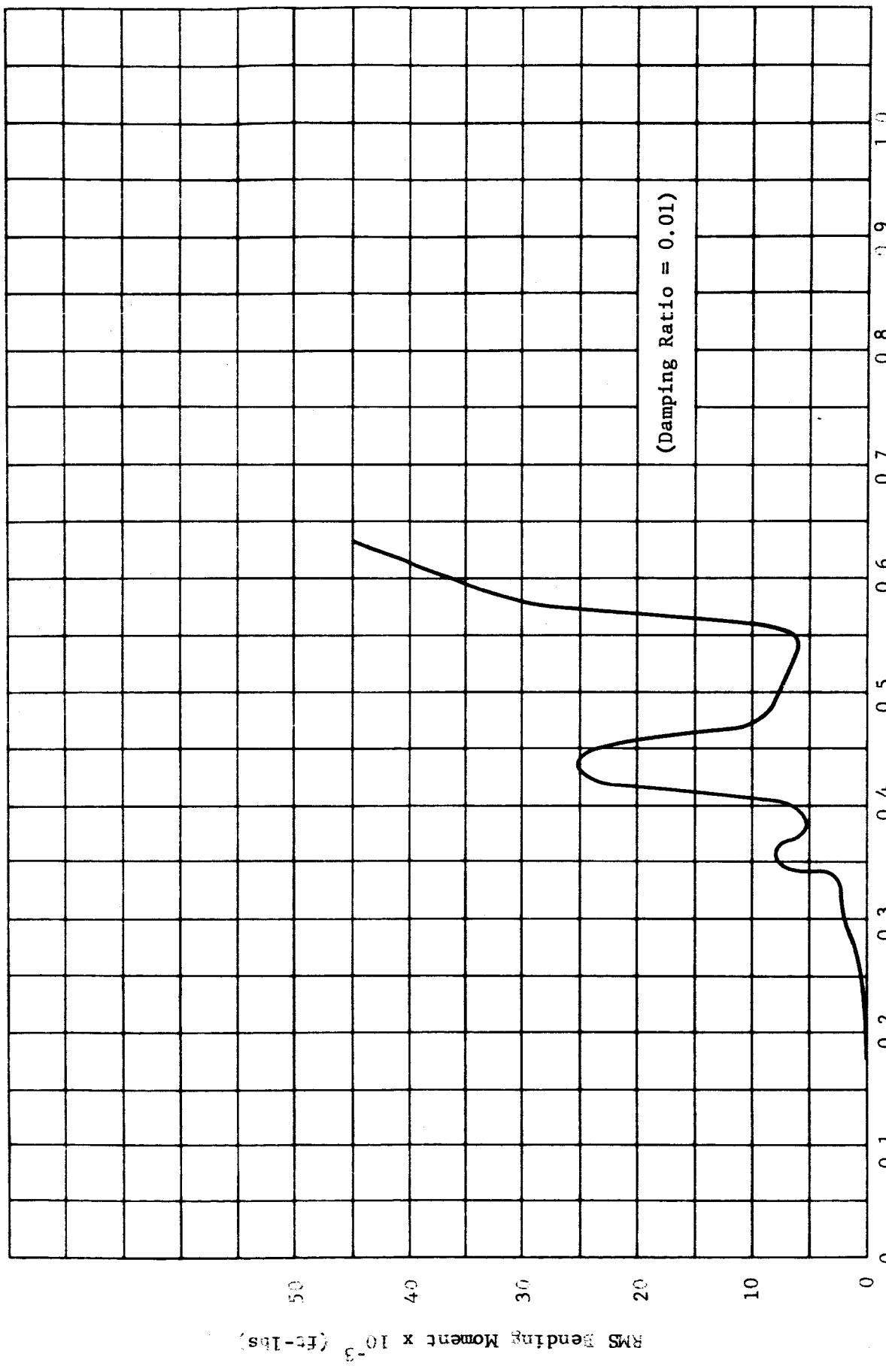


FIGURE 1. MINIMUM FULL SCALE RMS BENDING MOMENT CALCULATED FROM PSTL-1 TEST RESULTS, FOR MODE 1, BY CROSS SPECTRUM METHOD

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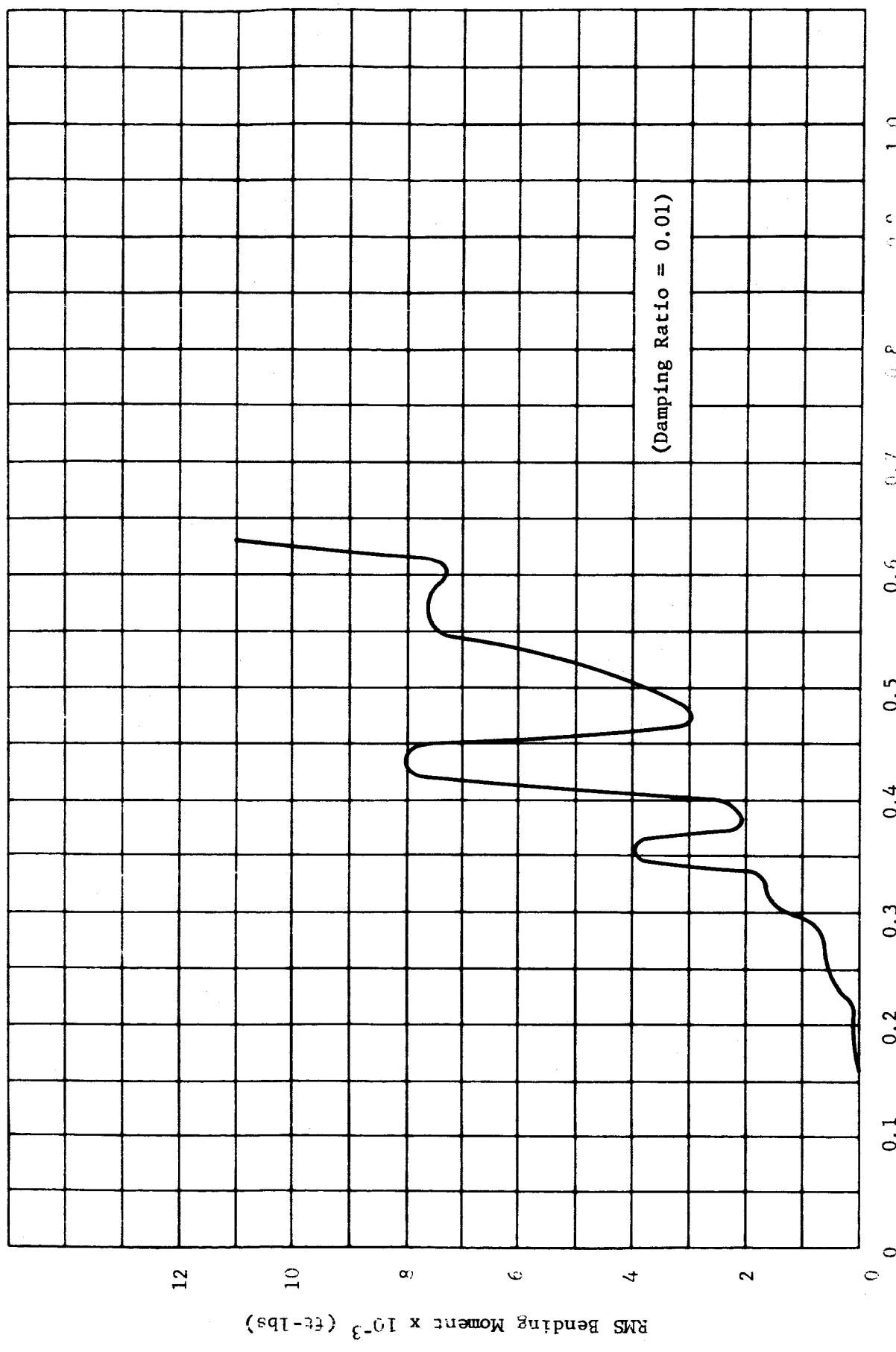


FIGURE 2. MINIMUM FULL SCALE SETTING MODES CALLED FROM SECTION M-T OF TEST RESULTS, FOR MOD. 2, 17 CROSS SECTION SLL-1

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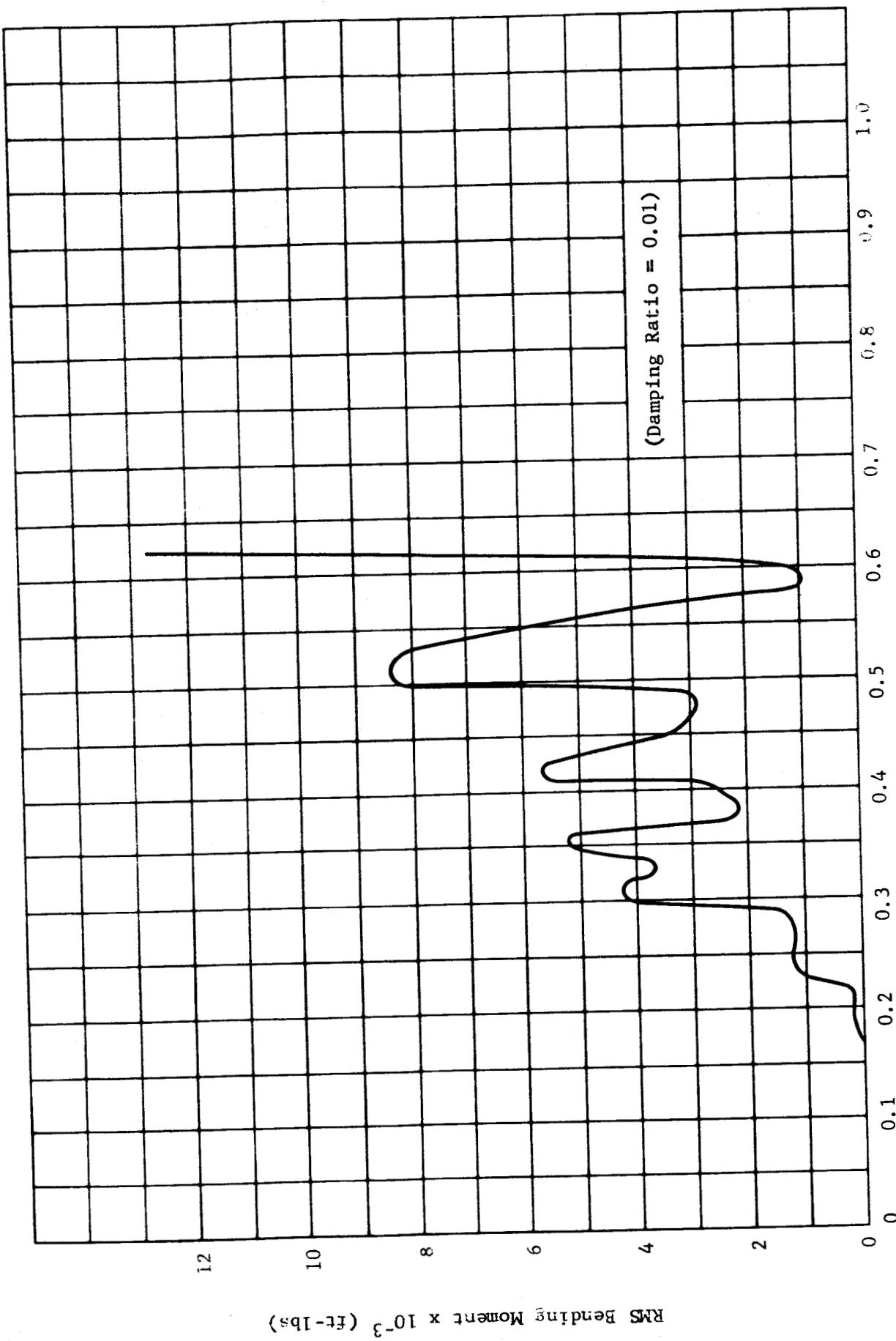


FIGURE 3. MINIMUM FULL SCALE RMS BENDING MOMENT CALCULATED FROM  $S_{LL-1}$   
TEST RESULTS, FOR MODE 3, BY CROSS SPECTRUM METHOD

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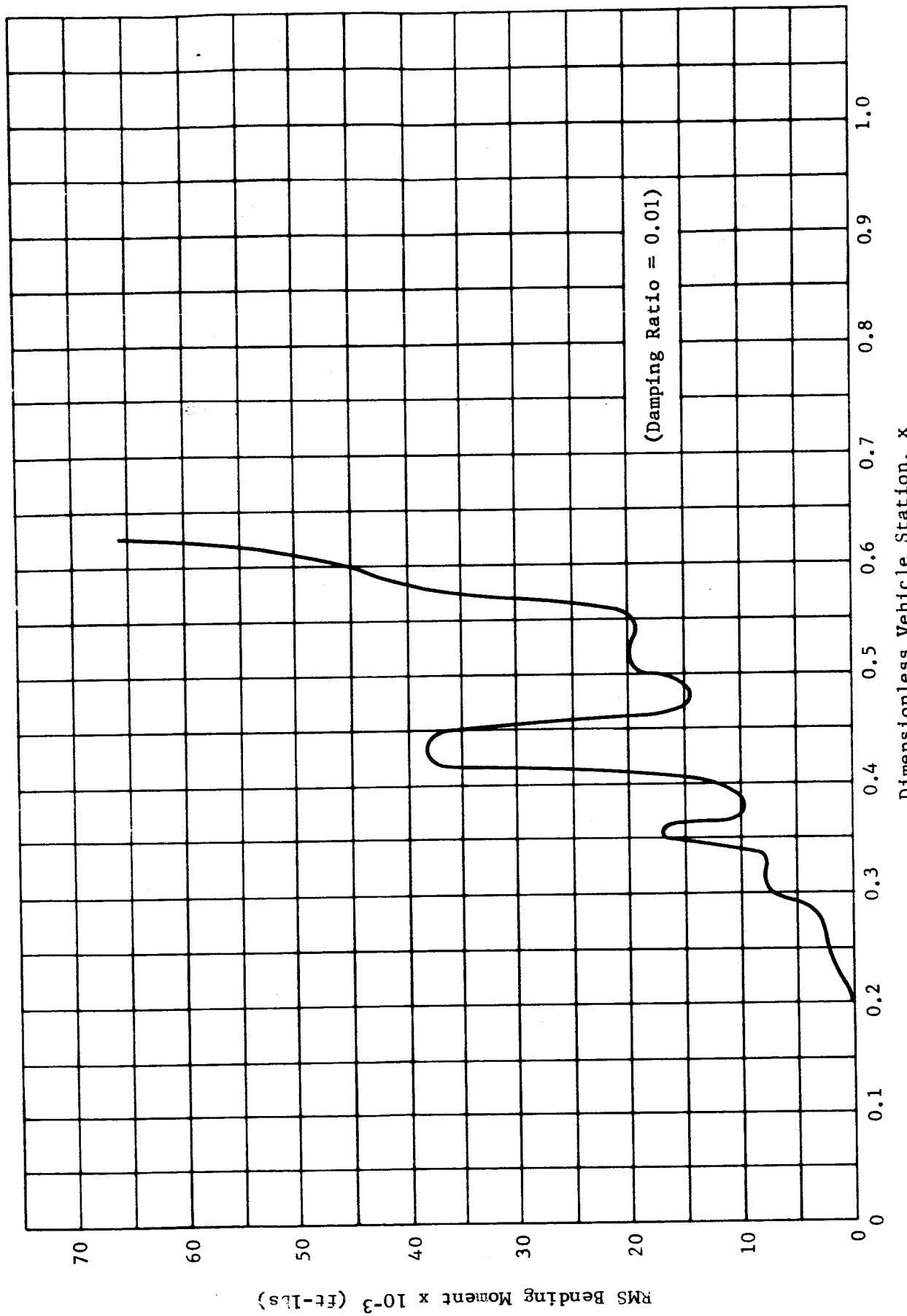


FIGURE 4. MINIMUM FULL SCALE RMS BENDING MOMENT CALCULATED FROM PSTL-1 TEST RESULTS, FOR THE TOTAL OF THE FIRST THREE MODES, BY CROSS SPECTRUM METHOD

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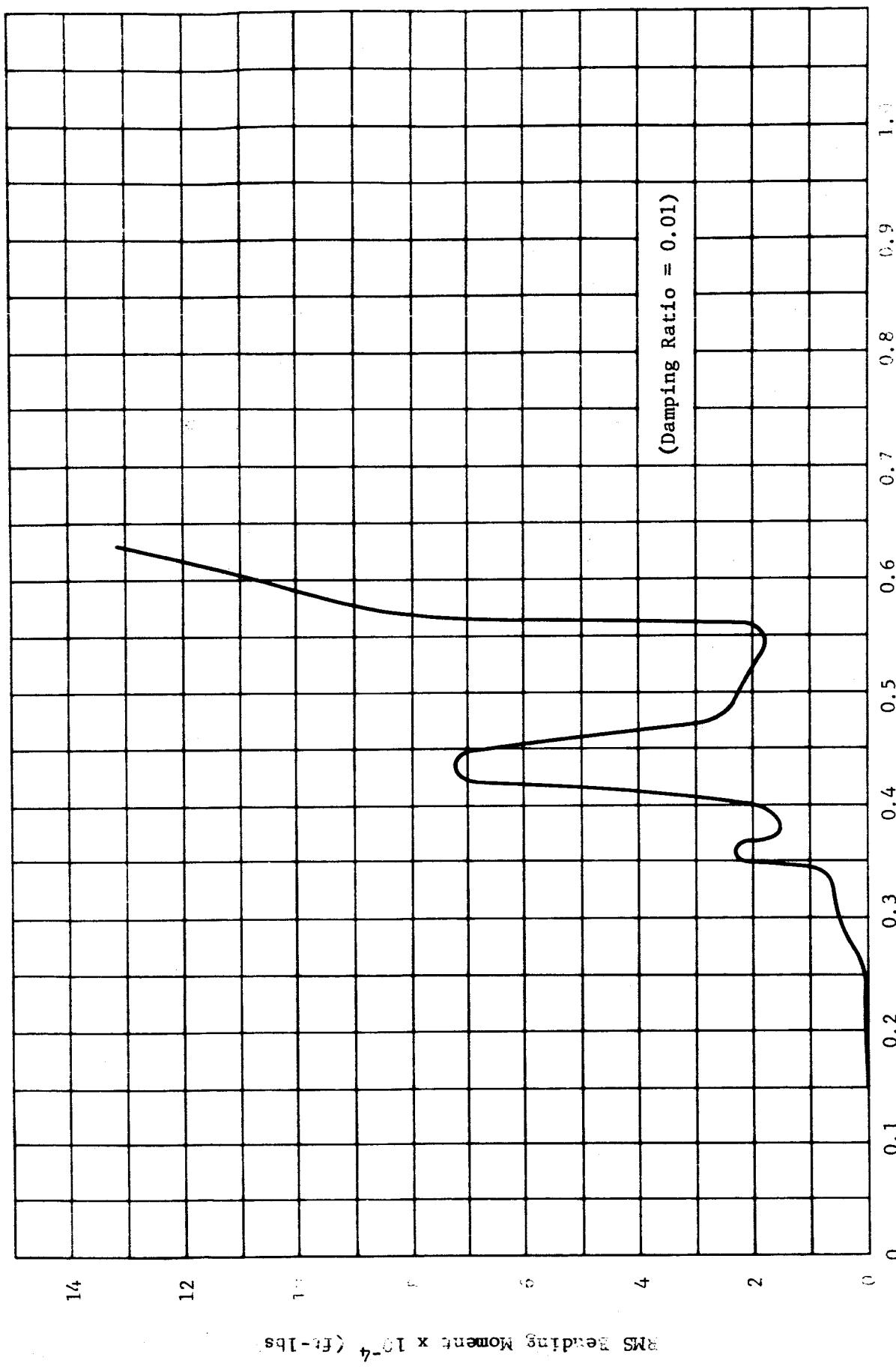


FIGURE 5. MAXIMUM FULL SCALE RMS BENDING MOMENT CALLED FROM TEST 1  
TEST RESULTS, FOR MOTION 1, BY CROSS SECTION METHOD

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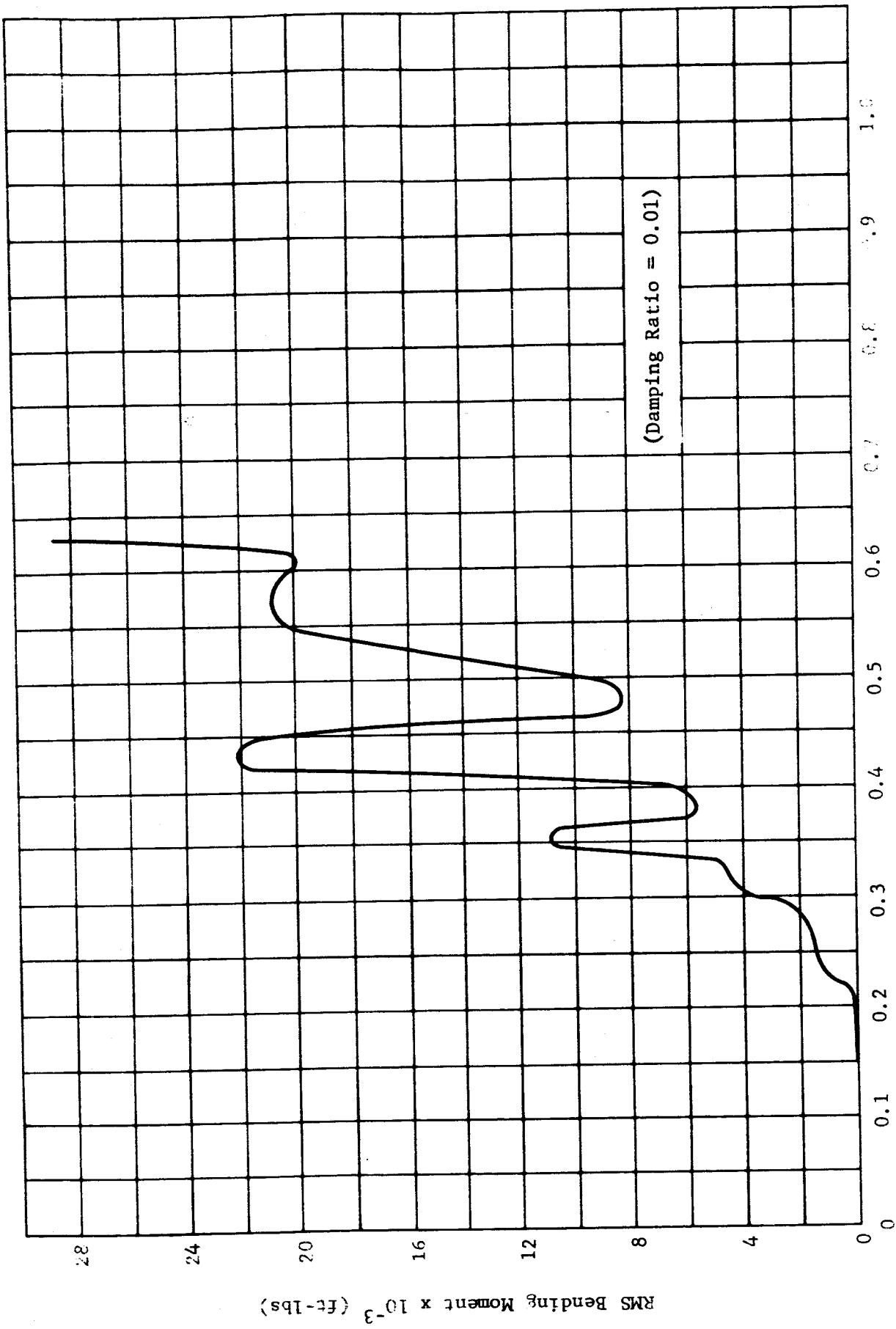


FIGURE 6. MAXIMUM FULL SCALE RMS BENDING MOMENT CALCULATED FROM TEST RESULTS, FOR MODE 2, BY CROSS SPECTRAL METHOD

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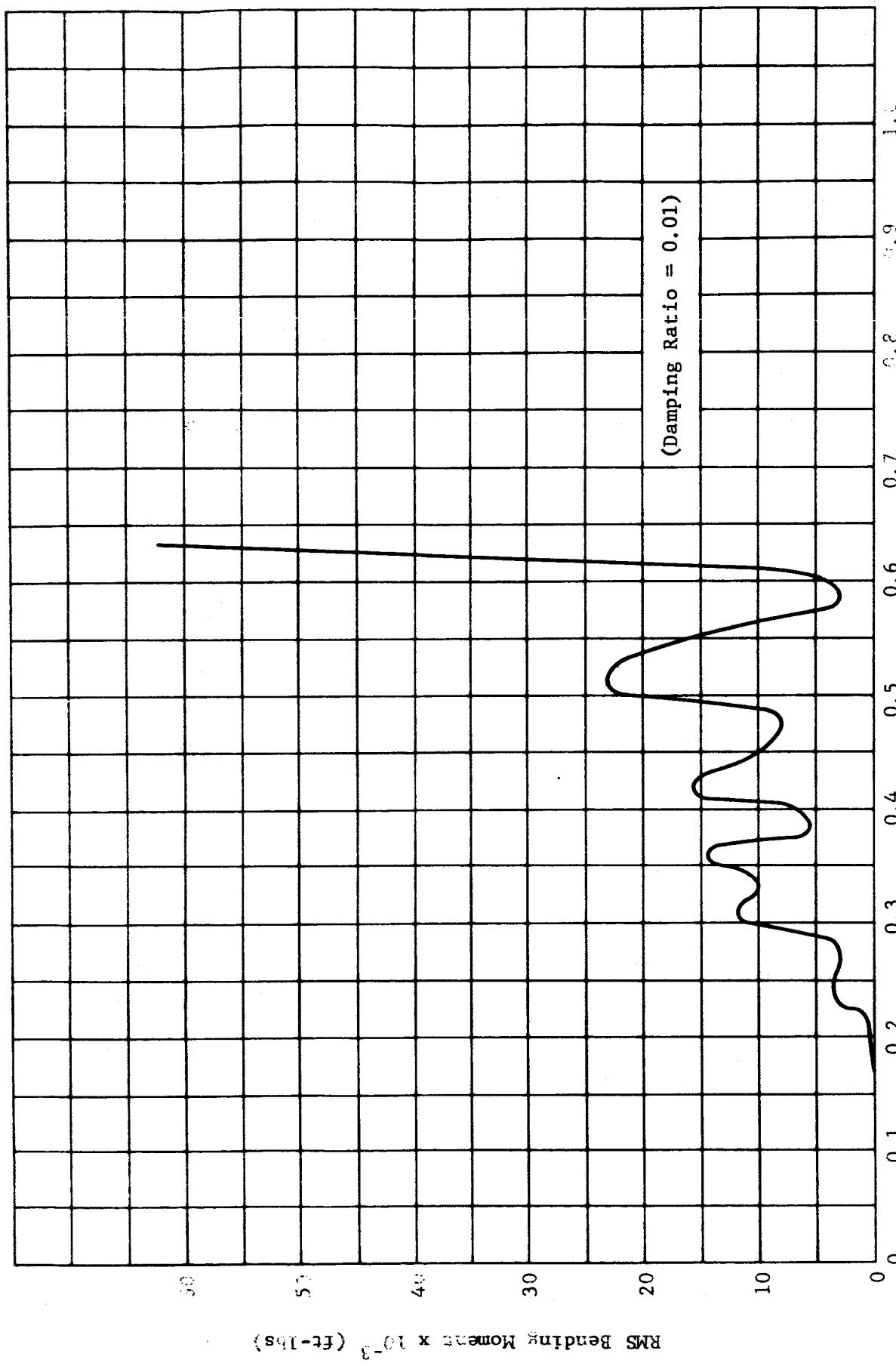


FIGURE 7. MAXIMUM FULL SCALE RMS BENDING MOMENT CALCULATED FROM TEST RESULTS, FOR MODE 3, BY GROSS SPECTRUM METHOD

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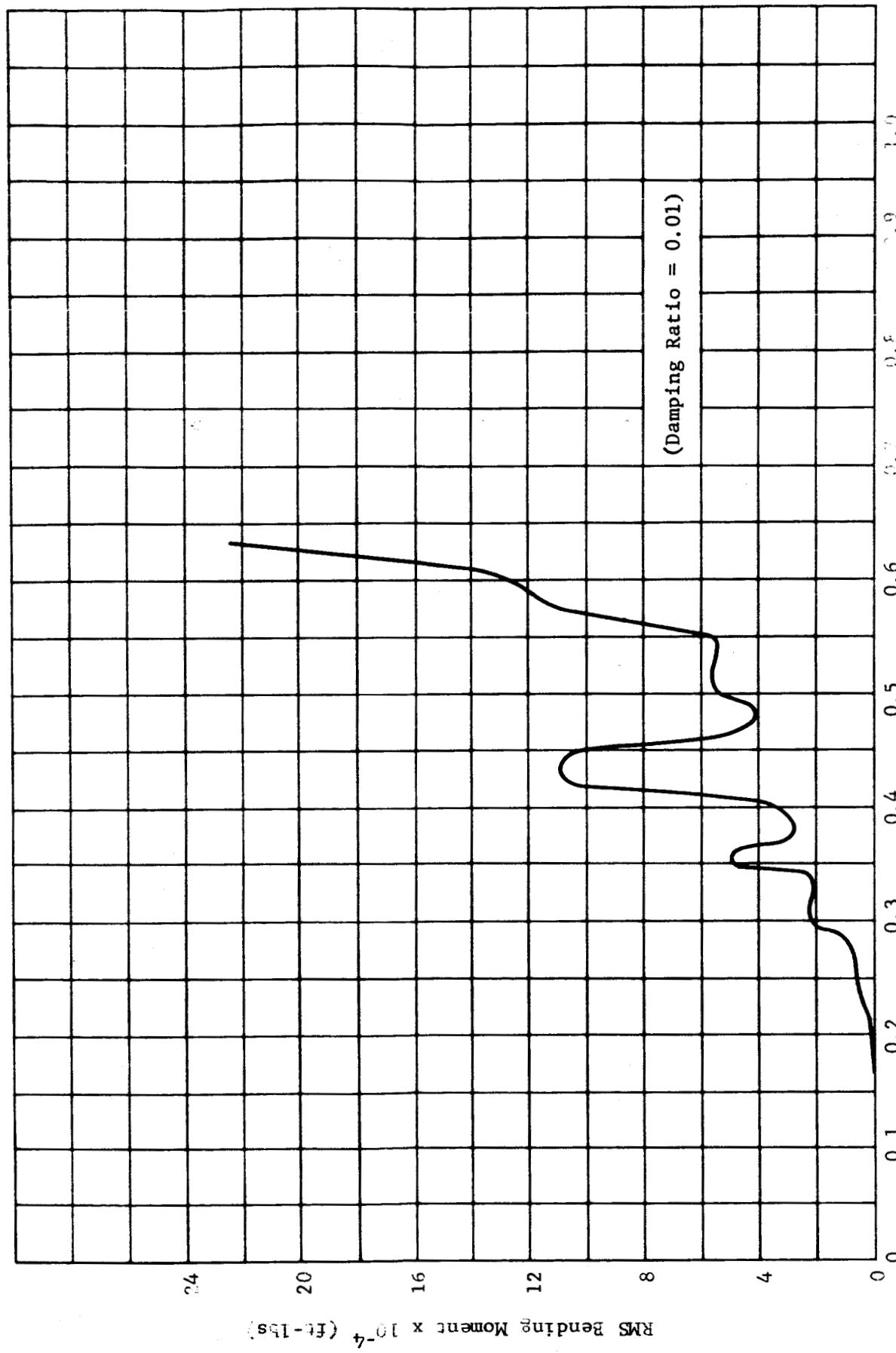


FIGURE 8. MAXIMUM FULL SCALE RMS BENDING MOMENT VARIATION VS. DIMENSIONLESS VEHICLE STATION FOR THE TOTAL OF FIVE TESTS OVER THE MOTION, BY CROSS SPECTRUM METHOD

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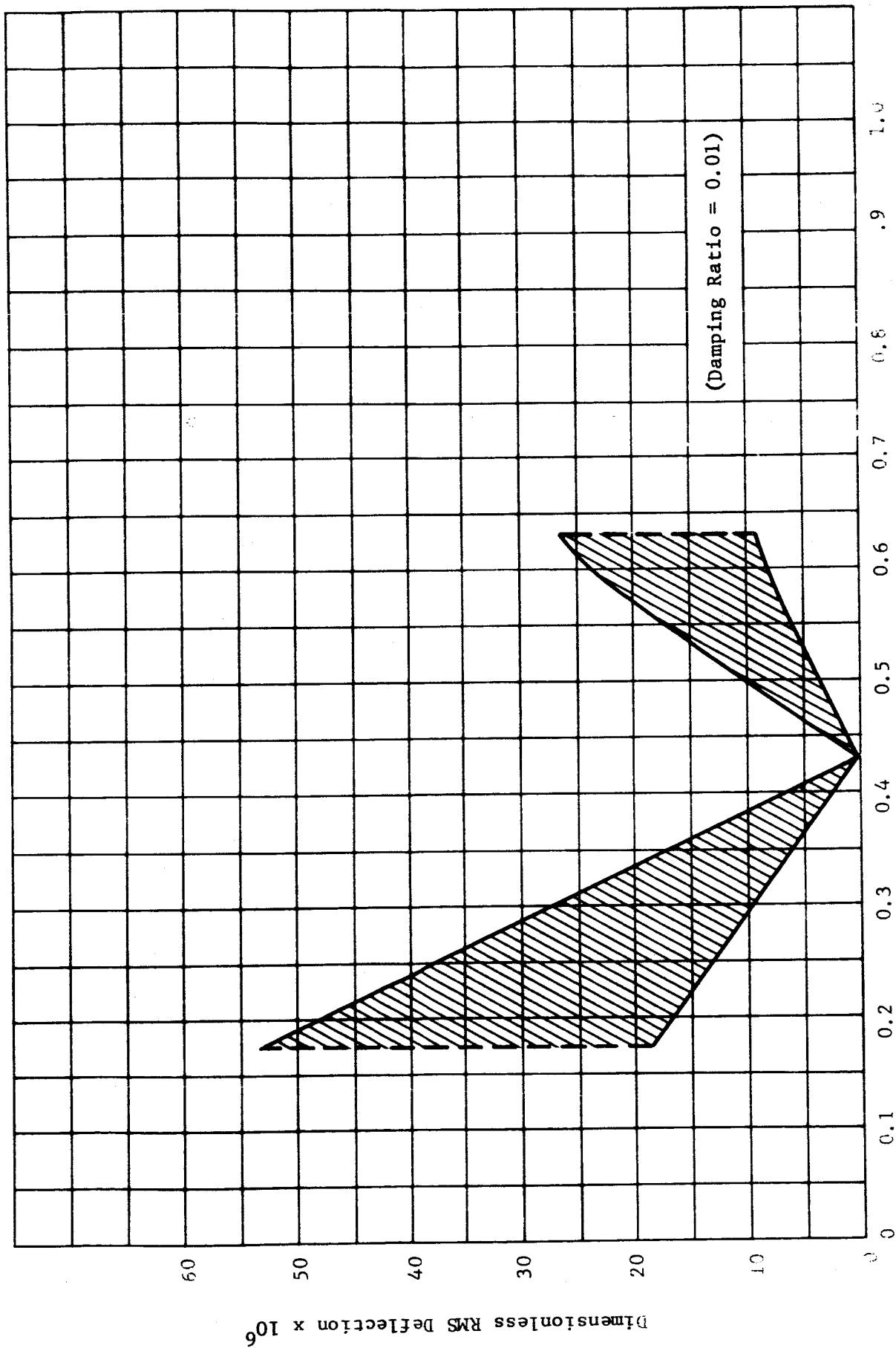


FIGURE 9. LIMITS OF FULL SCALE RMS DEFLECTION CALCULATED FOR MODE 1 TEST RESULTS, FOR MODE 1, BY CROSS SPECTRAL METHODS

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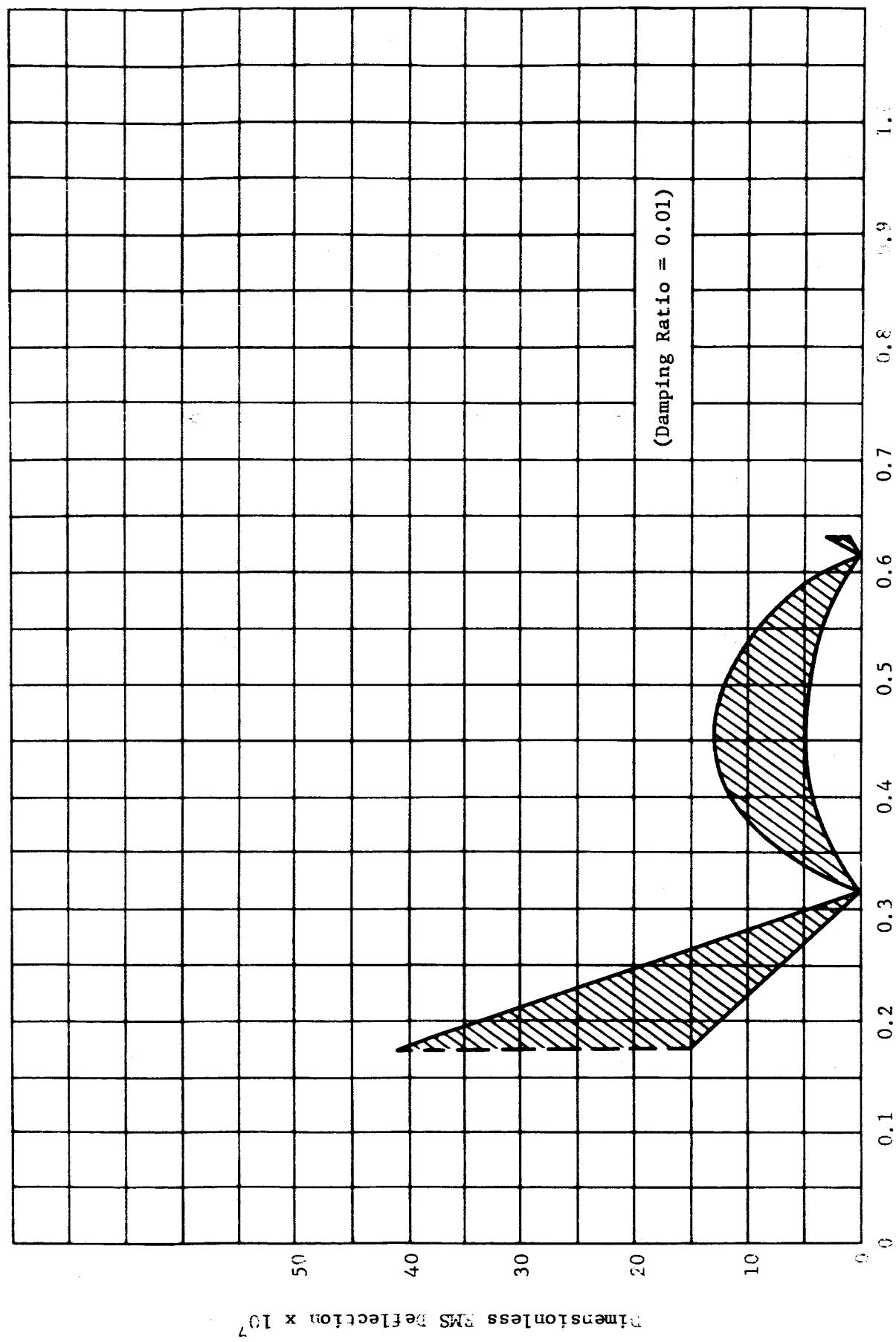


FIGURE 10. LIMITS OF FULL SCALE RMS DEFLECTION CALCULATION FOR MODE 2 TEST RESULTS, FOR MODE 2, BY CROSS SPECTRUM METHOD

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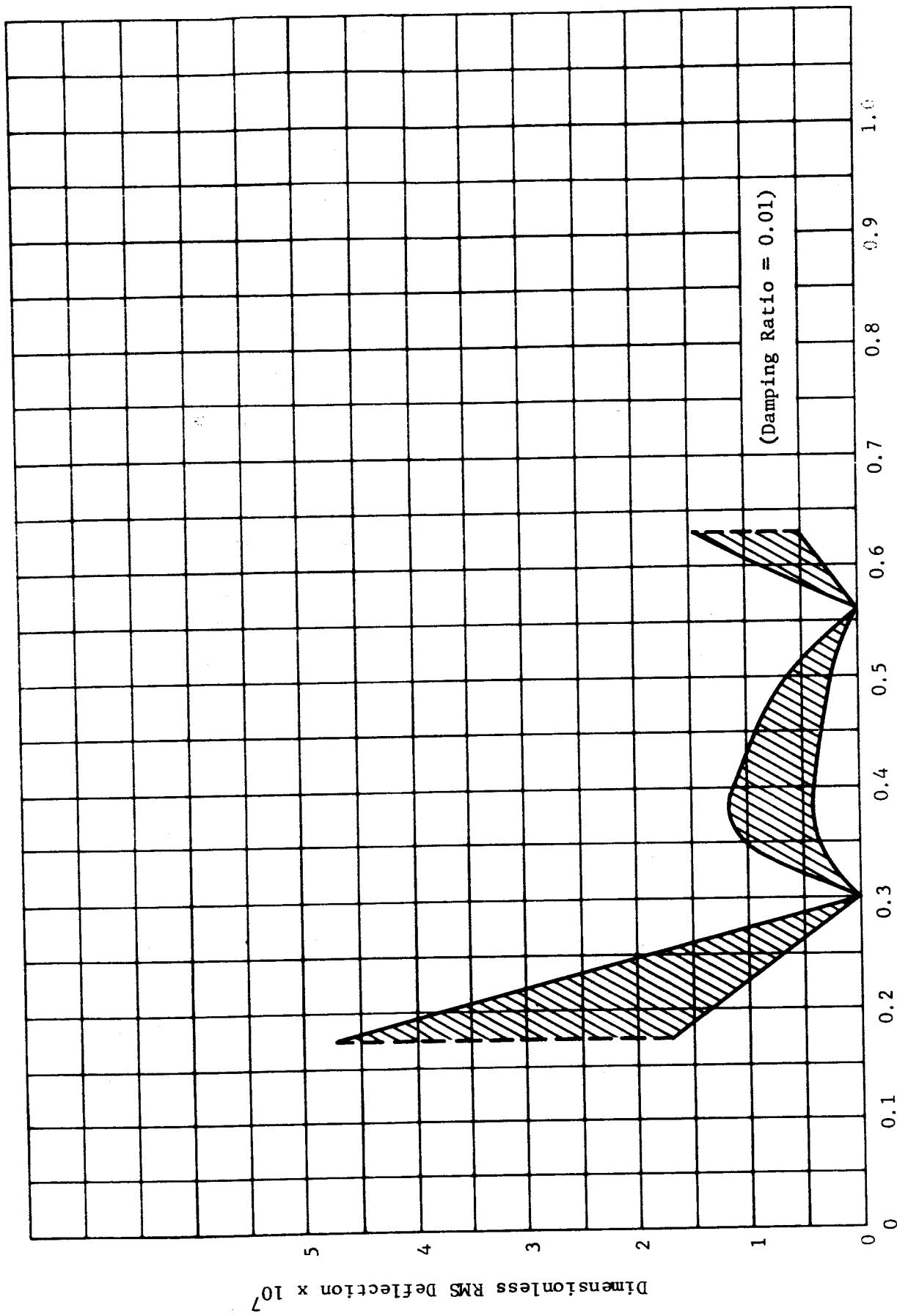


FIGURE 11. LIMITS OF FULL SCALE RMS DEFLECTION CALCULATED FROM STM-1 TEST RESULTS, FOR MODE 3, BY CROSS SPECTRUM METHOD

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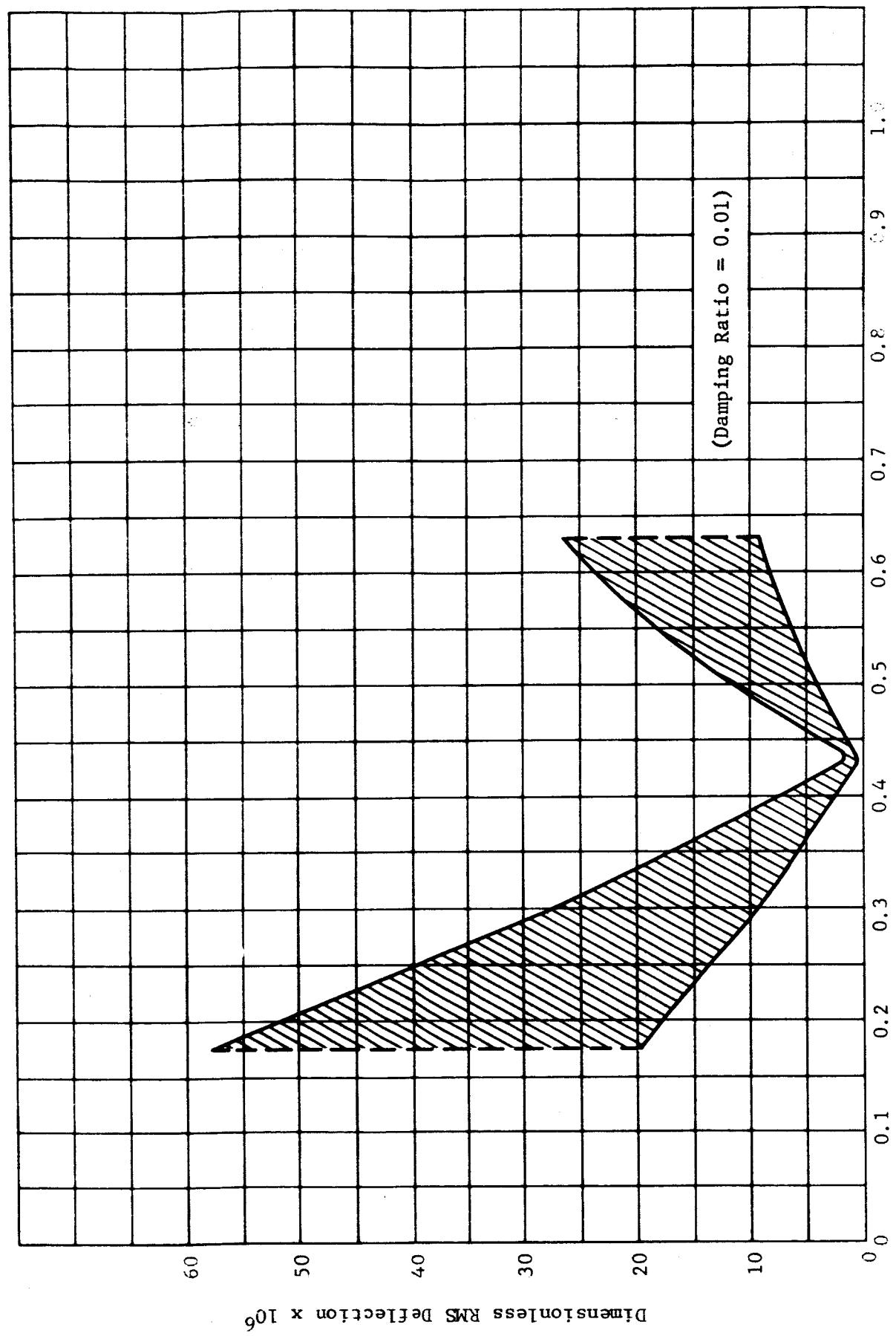


FIGURE 12. LIMITS OF FULL SCALE RMS DEFLECTION CALCULATED FOR ONE TEST RESULTS, FOR THE TOTAL OF THE FIRST THRE CROSS SPECTRUM METHOD

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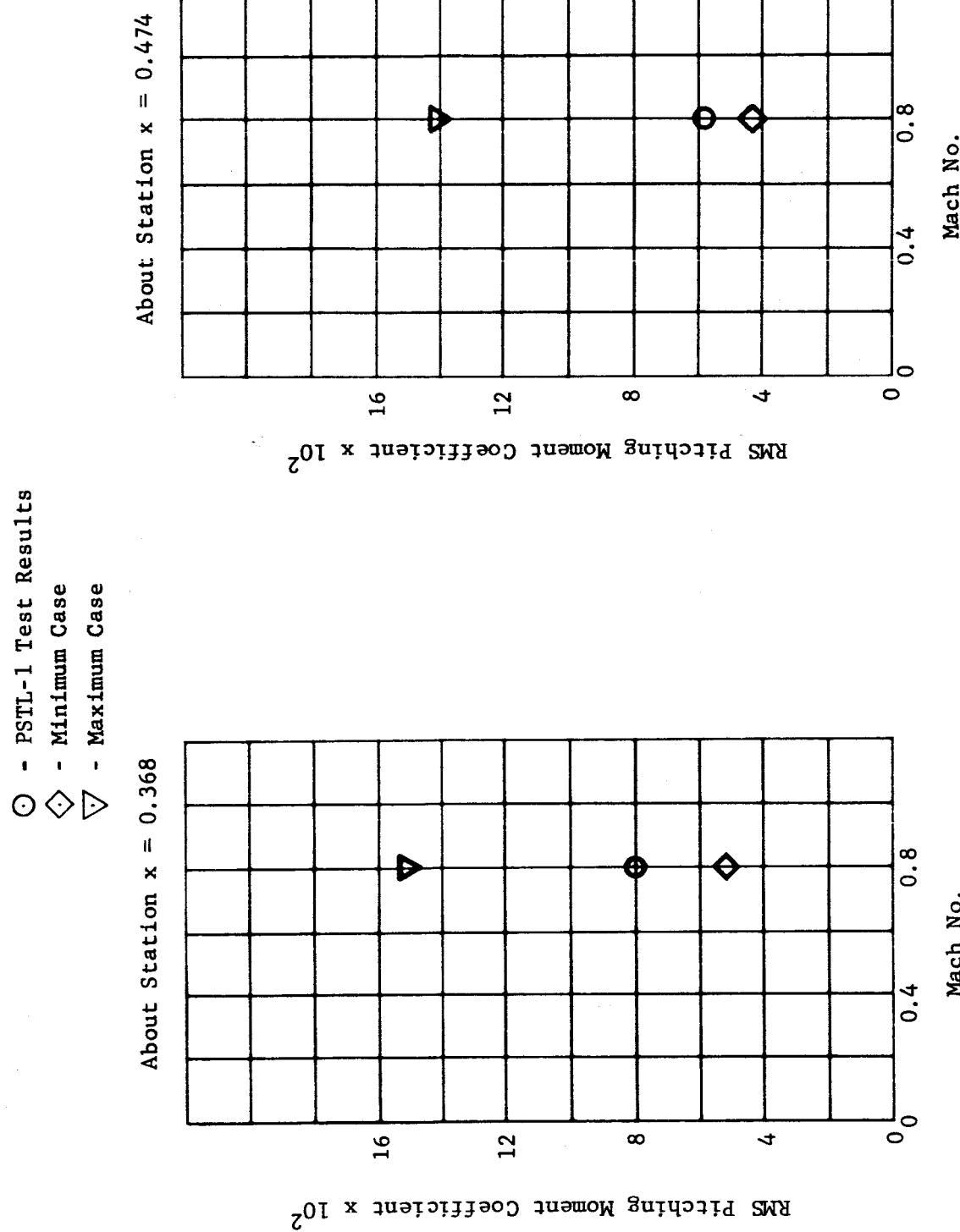


FIGURE 13. COMPARISON OF THE COMPUTED RMS PITCHING MOMENT COEFFICIENT WITH THE EXPERIMENTAL PSTL-1 COEFFICIENTS

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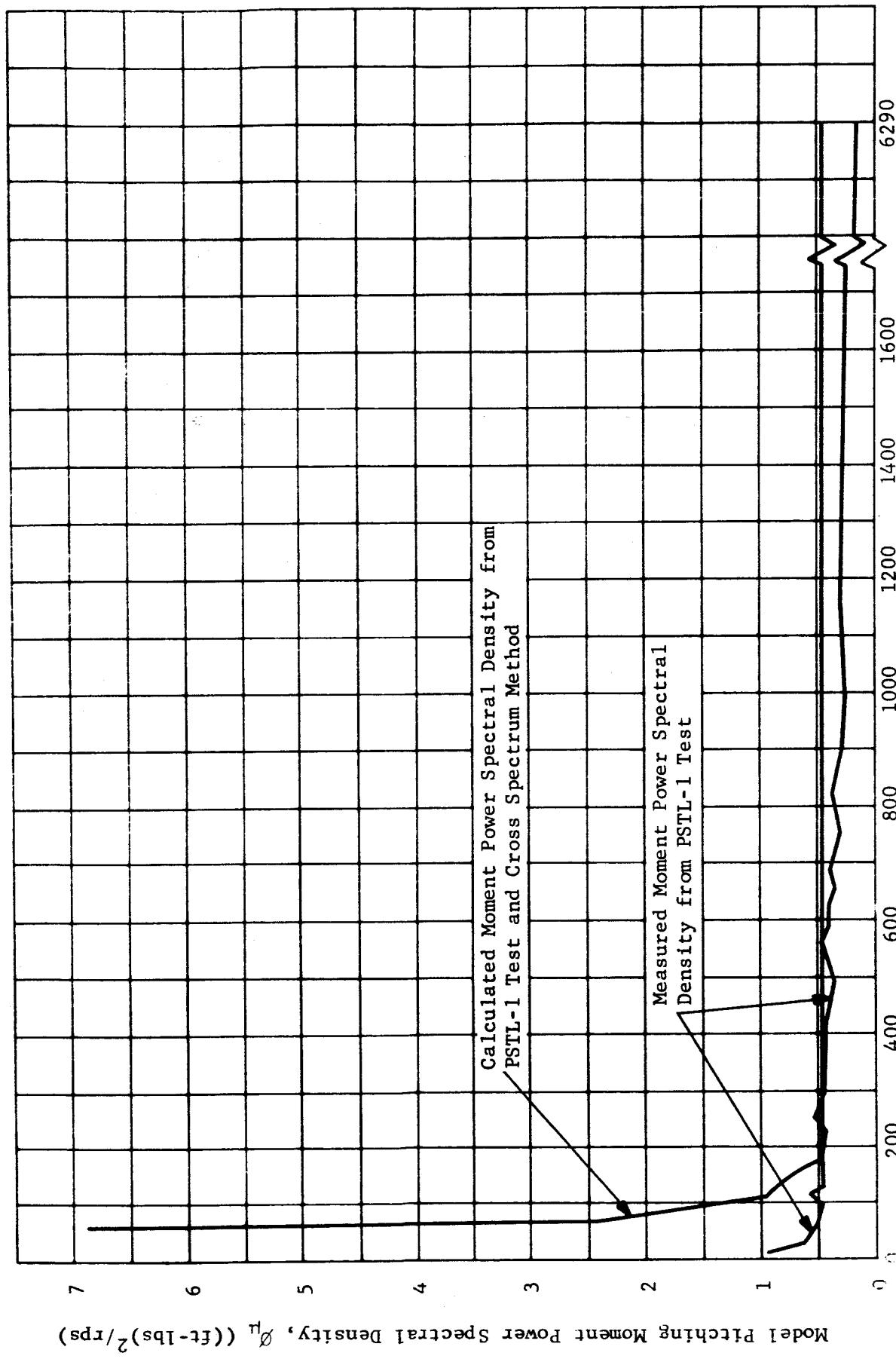


FIGURE 14. THE POWER SPECTRAL DENSITY OF THE CALCULATED AND MEASURED MOMENT FOR THE MAXIMUM CASE

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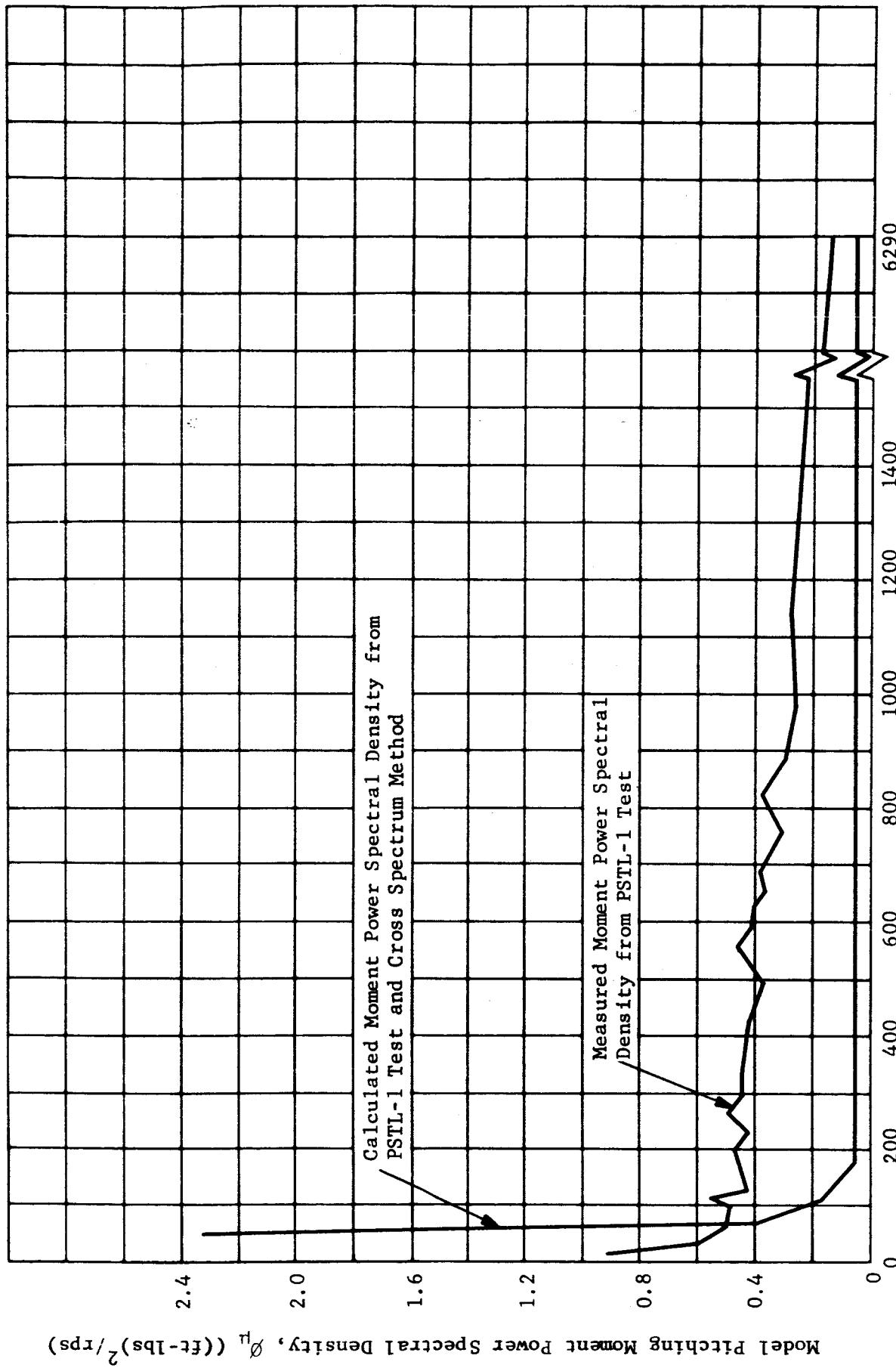


FIGURE 15. THE POWER SPECTRAL DENSITY OF THE CALCULATED AND MEASURED MOMENTS FOR THE MINIMUM CASE

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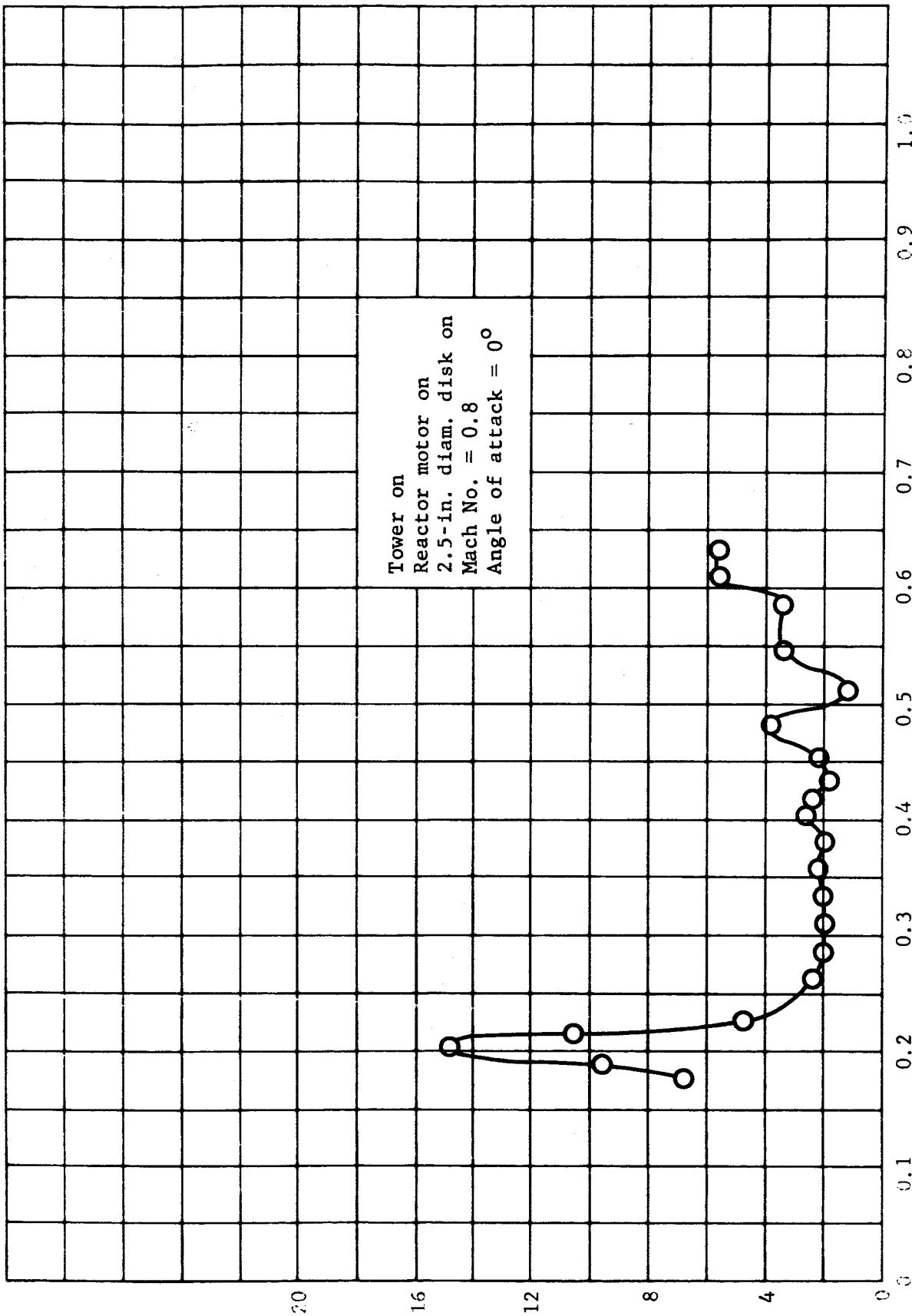


FIGURE 16. PSTL-1 RMS LOCAL NORMAL FORCE COEFFICIENT DISTRIBUTION

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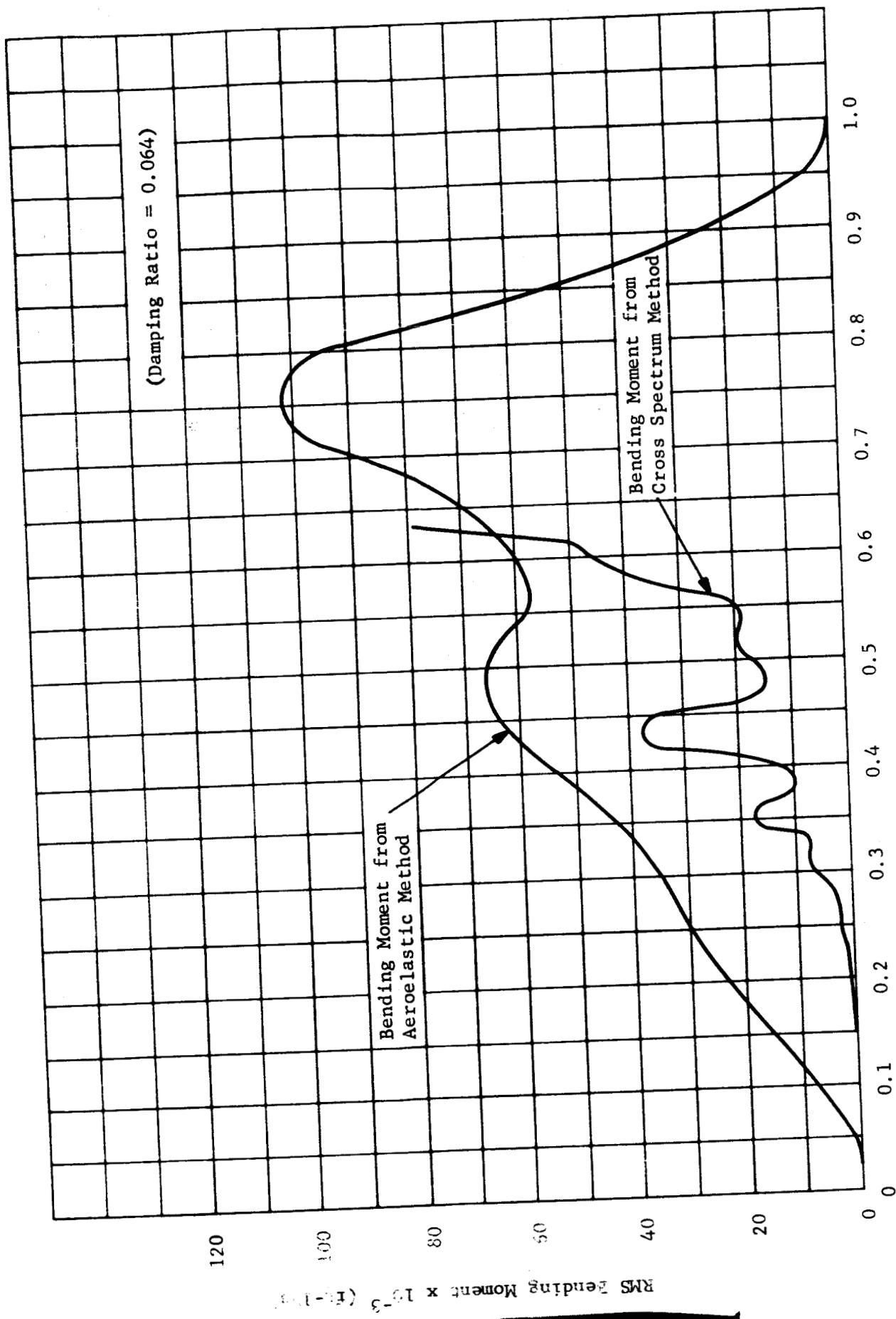


FIGURE 17. FULL SCALE PSTL-1 MINIMUM RMS BENDING MOMENT COMPARED TO THE AEROELASTIC RMS BENDING MOMENT

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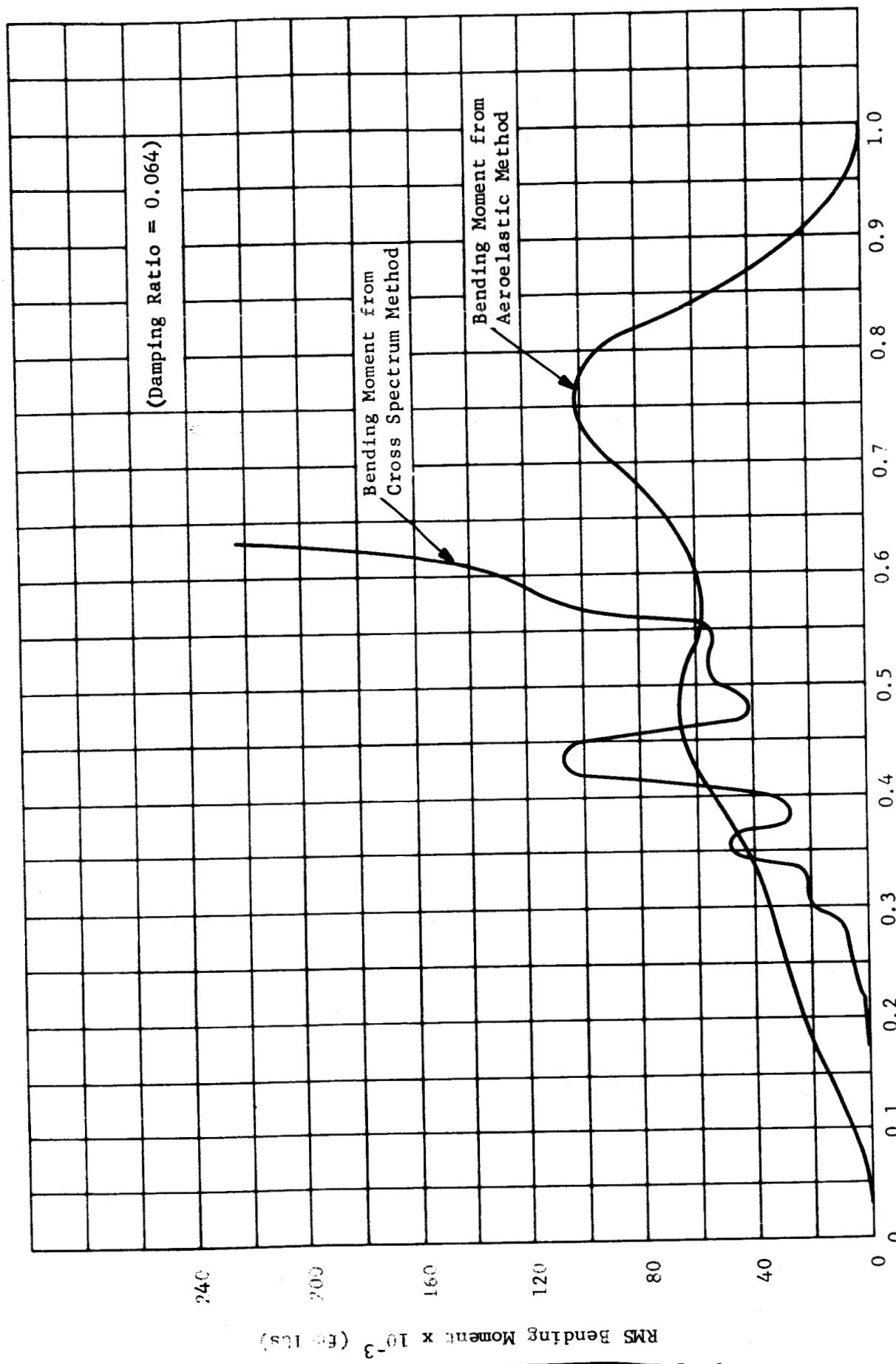
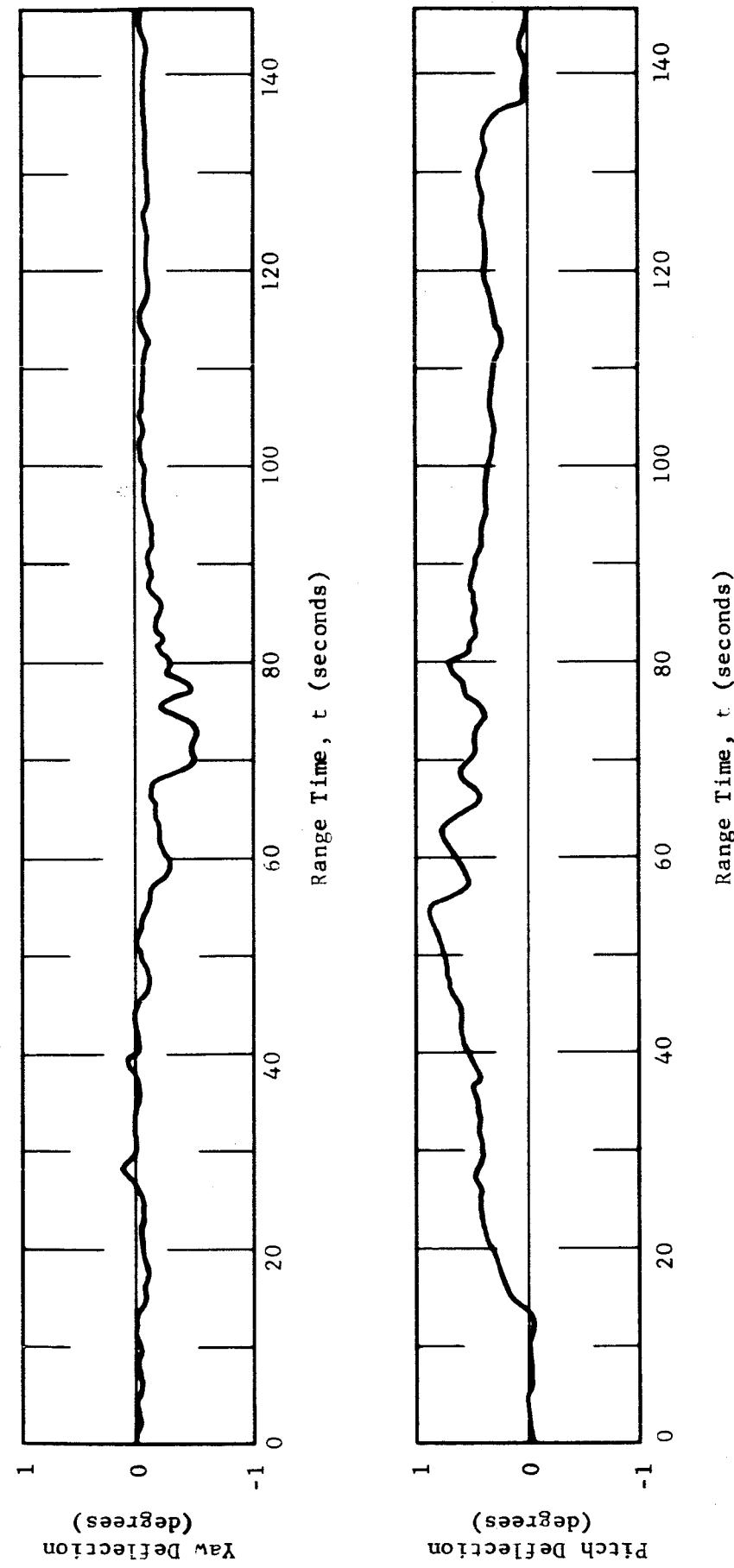


FIGURE 18. FULL SCALE PSL-1 MAXIMUM RMS BENDING MOMENT COMPARED TO THE AEROELASTIC RMS BENDING MOMENT

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The angular buffeting deflections at the I.U. calculated by cross spectrum method for Mode 1 are:

$$\left. \begin{array}{l} \text{Minimum case deflection} = 0.00344^\circ \\ \text{Maximum case deflection} = 0.0117^\circ \end{array} \right\} t = 57 \text{ sec}$$

FIGURE 19. FLIGHT DEFLECTION OF SA-7 AT THE INSTRUMENT UNIT

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